Research Paper Uncertainty Management in the Dynamics of Biological Systems: A Key to Goal-oriented Rehabilitation

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ABSTRACT

Introduction: Clean, noise-free data are ideal but often unattainable in biological control systems. Filters are usually employed to remove noise. But this process also leads to the loss or alteration of information. A considerable challenge is managing the uncertain knowledge using a proper and realistic mathematical representation and staying consistent with biological patterns and behaviors. This study explores the potential of fuzzy logic as a computational paradigm to manage uncertainties in the nonlinear dynamics of human walking. This field has paid little attention to this aspect despite its considerable nonlinear and uncertain behavior due to adaptability, muscle fatigue, environmental noise, and external disturbances.

Methods: We employed a fuzzy logic-based controller integrated with functional electrical stimulation (FES) and a gait basin of attraction concept to enhance gait performance. Our controller focused on accommodating imprecision in shank angle deviation and angular velocity rather than relying on predetermined trajectories.

Results: Our findings indicate that more fuzzy rules and partitions improve the similarity of the gait dynamics to those of a healthy human. Moreover, higher membership function overlaps lead to more robust gait control.

Conclusion: The study demonstrates that fuzzy logic can effectively manage uncertainties in the nonlinear dynamics of human walking, improving gait performance and robustness. This approach offers a promising direction for goal-oriented rehabilitation strategies by mimicking the human mind's ability to handle challenging and unknown environments.

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Highlights

- Managing uncertainty improves gait without exoskeletons or set paths.
- The proposed fuzzy-based approach enhances gait control by managing uncertainties.
- Increasing fuzzy rules and partitions improves gait dynamics.
- More membership function overlap leads to more robust gait control.
- Effective management of uncertainty can revolutionize rehabilitation.

Plain Language Summary

Walking and maintaining balance is a complex process influenced by muscle fatigue: environmental noise, and various disruptions. How a person walks is generally referred to as a movement pattern, and in rehabilitation, the main goal is to create a movement pattern similar to that of a healthy person in individuals with movement disorders. Achieving this goal depends significantly on our approach to designing treatment and control strategies. To effectively control such behavior, we need a control strategy that interacts with the nonlinear nature of the system rather than simply tracking a predetermined path while always maintaining a holistic view. This strategy must manage existing uncertainties and imprecise knowledge in system dynamics while aligning with the desired goal. Among various control strategies, fuzzy logic stands out because it mimics the human mind's ability to manage fuzzy and imprecise knowledge, making it particularly suitable for handling the complexities of biological systems such as walking. In this study, we investigate the potential of fuzzy logic to address this challenge by creating a synergy between a fuzzy controller and the identified mapping related to the shank dynamics, which serves as the input for this controller.

1. Introduction

he modern dormant lifestyle, injuries, and strokes have increased incidents of walking disorders. However, the brain can reorganize itself and make adaptive changes, known as neural plasticity (Ding et al., 2005; Johansson, 2007). Hence, there is

a possibility for walking healthily again with an effective rehabilitative and muscle-strengthening program. To this end, functional electrical stimulation (FES) is often considered a viable neurorehabilitation technology. However, devising an effective FES-based control strategy could be very complex and uncertain due to human gait rehabilitation's unknown and time-varying dynamics. Robotic devices used concurrently with FES are also suggested to assist with diverse sensory and motor functions (Díaz et al., 2011; Shi et al., 2019; Zhou et al., 2021; Viteckova et al., 2013). For instance, Andrews et al. (1988) used a hybrid FES orthosis for patients with spinal cord damage paraplegic in cases where the quadriceps muscles were electrically excitable. Nevertheless, the common concern in such rehabilitation programs remains to find a suited control strategy (Marchal-Crespo & Reinkensmeyer, 2009; Meng et al., 2015; Foroutannia

et al., 2022), with the added complexity of choosing the proper combination of electrical stimulation and robotic devices (Brunetti et al., 2011; Del-Ama et al., 2014; Kimura et al., 2018).

So far, diverse control methods have been designed to restore movement and gait correction in patients with movement disorders. These studies suggest that using the traditional trapezoidal stimulation intensity approach is inappropriate due to its incompatibility with the muscle activity patterns in healthy walking. In contrast, a stimulation strategy based on the natural muscle activation patterns could improve walking in disorders such as foot drop. FES performance could also improve while reducing muscle fatigue and energy consumption (Lyons et al., 2000; O'Keeffe et al., 2003). Furthermore, to correct foot drop, we can use an algorithm to predict step frequency for applying excitation close to natural walking by simulating natural patterns from the EMG dataset of the anterior tibialis muscle (Chen et al., 2013). A sliding-mode controller, in which an adaptive fuzzy controller compensates for approximation errors, is suggested for paraplegic patients. In this case, the control strategy guarantees accurate tracking, leading to muscle excitation patterns similar to normal gait and fast con-



Figure 1. The bipedal model showing the angles: Joints and muscles

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vergence (Nekoukar & Erfanian, 2011). Furthermore, a decoupled controller structure, i.e. separately for each joint-muscle dynamics, is suggested by Nekoukar and Erfanian (2012) that consists of an adaptive fuzzy terminal sliding mode controller to adjust the pulse width of the stimulation signal and a fuzzy controller to adjust the pulse amplitude of the excitation signal.

Partial and decoupled handling of joints and using predetermined trajectories are not the appropriate framework for a biological system's real-world uncertainties and complex dynamics. Instead, a suitable control strategy should carry a holistic view by operating around a stable walking phase space manifold (Fu et al., 2014). This objective, however, is non-trivial due to biological systems' time-varying and complex and uncertain dynamical behavior. In other words, an ill-defined problem is posed here since the exact equations of the system and its saddle cycle in the gait phase space and its manifolds are unknown.

It is important to note that the objective of rehabilitation extends beyond merely generating movement in a disabled limb. Sometimes, purely mimicking movement without considering the dynamics of the system and the inherent synergy between muscles and joints can be detrimental. Moreover, human knowledge regarding various aspects of the surrounding world is limited, leading to simplification and modeling of phenomena like walking. However, this simplification and modeling process can increase uncertainty, potentially diverting us from the ultimate goal. Now, the significance of employing the correct approach to address uncertainties in the dynamics of biological systems becomes apparent, particularly in goal-oriented rehabilitation. By understanding and effectively dealing with these uncertainties, we can direct our efforts toward the creation of rehabilitation methods that are purposeful and aimed at achieving the desired outcomes.

This study aims to exploit this (tolerance for) uncertainty and imprecision to enhance the quality of gait rehabilitation. Specifically, we employ a fuzzy controller using a gait basin of attraction (Rezaee & Kobravi, 2020) and study how its uncertainty representation influences gait performance. The controller's inputs are the commonly measurable shank angle and shank angular velocity's deviation from a detected sine-circular map, and its output is the excitation signal.

The remainder of this report is organized as follows. The materials and methods include the human walking model, the data acquisition process, the control strategy, and simulations and analysis. Finally, the overall results and conclusions are presented in the results and discussion.

2. Materials and Methods

Human walking model

A bipedal musculoskeletal model was used for this study (Figure 1). In the musculoskeletal model used for simulation, the ankle and phalangeal joints are not explicitly considered, assuming the subject uses an ankle-foot orthosis while walking. By stabilizing the lower limb and correcting alignment, the orthosis allows the focus to remain on the dynamics of the knee and hip joints, thereby approximating a gait pattern that resembles normal walking. The integration of FES and orthosis effectively compensates for the simplified joint model. The orthosis stabilizes the lower limb and supports a natural walking pattern, while FES ensures that the knee and hip muscles are appropriately engaged. This combination enables the study to approximate healthy gait patterns despite modeling only two joints.

Equation 1 describes the model dynamics,

1. M
$$\ddot{x}(t)$$
+C $\dot{x}(t)$ +G+ τ_{fd} = $\tau(t)$ +V(t)

, where X(t)=[x_K x_H]^T represents the angles vector (i.e. x_K and x_H are the knee and hip joint angles, respectively). Also, X'(t)=[x_K x'_H]^T indicates the angular velocity of the knee and hip joints. M is the inertia matrix, C is the Coriolis torque matrix, G is the gravity force vector, τ_{fd} is a vector of ground reaction torque, and V(t) is the white noise, which expresses the uncertainty process.

 $T(t)=[\tau_s \tau_T]^T$ is the torque vector produced in the shank and thigh determined as follows:

$$\tau_i(t) = \tau_i^{f}(t) - \tau_i^{e}(t) - \tau_i^{r}(t)$$

i=k, H

2.

 $\tau_{s}(t) = -\tau_{\kappa}(t)$

$$\tau_{\mathrm{T}}(t) = \tau_{\mathrm{K}}(t) + \tau_{\mathrm{H}}(t)$$

, where the parameters T_i^f , T_i^e , and T_i^r are flexor, extensor, and resistance torques, respectively, described as:

$$\tau_{i}^{j}(t) = (c_{i2}^{j} x_{i}^{2} + c_{i}^{1} l^{j} x_{i}^{+} + c_{i}^{0} l^{j}) \cdot g_{i}^{j}(x_{i}^{-}) \cdot a_{i}^{j},$$
3.

$$i \in \{k, H\} \qquad j \in \{f, e\}$$
4.
$$\tau_{K}^{r}(t) = d_{11} (x_{K} - x_{K0}) + d_{12} x_{K}^{-} + d_{13} e^{(d14 xK)} - d_{15} e^{(d16 xK)}$$
5.
$$\tau_{H}^{r}(t) = d_{21} (x_{H} - x_{H0}) + d_{22} x_{H}^{-} + d_{23} e^{(d24 xH)} - d_{25} e^{(d26 xK)}$$

The variables g^{*j*} are determined as:

$$g_i^f(\dot{x}_i) = \begin{cases} b_{i1} & \dot{x}_i < \frac{1 - b_{i1}}{b_{i2}^f}, \\ 0 & \frac{1}{b_{i2}} \le \dot{x}_i, \\ 1 - b_{i2}\dot{x}_i & \frac{1 - b_{i1}}{b_{i2}} \le \dot{x}_i < \frac{1}{b_{i2}}, \end{cases}$$

6.

$$g_i^e(\dot{x}_i) = \begin{cases} b_{i4} & \frac{b_{i4-1}}{b_{i3}} \le \dot{x}_i, \\ 0 & \dot{x}_i \le \frac{-1}{b_{i3}}, \\ 1 + b_{i3}\dot{x}_i & \frac{-1}{b_{i3}} \le \dot{x}_i < \frac{b_{i4-1}}{b_{i3}} \end{cases}$$

The variables a_i^j in Equation 3 indicate the activity of flexor and extensor muscles that are determined as below:

7.
$$\dot{a}_{j}^{i} = \begin{cases} [u_{i}/\tau_{act} + (1-u_{i})/\tau_{deact}](u_{i}-a_{i}) & u_{i} \geq a_{i}, \\ (u_{i}-a_{i})/\tau_{deact} & u_{i} < a_{i}, & i = 1,2,3,4, \end{cases}$$

, where the variables u_i are the normalized output signals of the controller, which are applied to the four muscles involved in gait in this model (i.e. flexor and extensor muscles of the hip and knee joints). The values of the parameters τ_{act} and τ_{deact} , which are time constants of activation and deactivation, respectively, 20 and 60 ms are adjusted.

Further details and adjustments of the values of the parameters are described in some studies (Nekoukar & Erfanian, 2011; Dosen & Popovic, 1999; Kimura et al., 2009).

Data acquisition

In this study, we used the data from Rezaee and Kobravi (2020) study. The present analysis uses shank angle data of 5 healthy volunteers during three uninterrupted gait cycles. Specifications of volunteers are given in Table 1. Also, Figure 2 shows the markers' position for tracking the shank movement during gait and data acquisition.

Control strategy

In this study, four main steps are taken to design the controller. The first step is to plot and reconstruct the phase space of the system based on drawing the shank angle, the shank angular velocity, and the shank angular acceleration relative to each other (Figure 3).

The second step is to apply the Poincaré section in the gait phase space to collect points that contain essential information about gait dynamics (Figure 4). In this research, the method of computing the normal vector is used to get the Poincaré section equation (Rezaee & Kobravi, 2020).

The third step is to select a proper map describing the relative variations of the collected points by the Poincaré section. The walking process has a cyclical behavior, and its basin of attraction can have periodic, quasi-periodic, or chaotic characteristics.

Hence, we used the sine-circle map because it can describe these features. Equation 8 defines the sine-circle map where θ is the desired parameter, Ω represents the frequency rate, and K determines the degree of nonlinearity (Jensen et al., 1960; DeGuzman & Kelso, 1991;

Variables	Gender	Age (y)	Height (m)
Sub1	Female	24	1.68
Sub2	Female	24	1.65
Sub3	Female	26	1.75
Sub4	Female	29	1.68
Sub5	Male	23	1.78

Table 1. Characteristics of the participants (Rezaee & Kobravi's, 2020)

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Note: The subjects were asked to walk at their normal walking speed. Datasets are acquired by the motion analyzer system (Qualisys product) with a recording frequency of 100 Hz.

Hilborn, 2000). Ω and K are estimated using the least square error method (Rezaee & Kobravi, 2020).

8. $\theta_{n+1} = \theta_n + \Omega - K/2\pi \sin(2\pi\theta_n)$,

To simplify the structure of the controller, only two maps identified in the study (Rezaee & Kobravi, 2020), which are related to the shank angle and angular velocity, have been used.

Equation 9 shows two identified maps where X_s is the shank angle, and X_s is the shank angular velocity.

$$X_{s}(n) = X_{s(n-1)} + \Omega_{1} - K_{1}/2\pi \sin(2\pi X_{s(n-1)})$$
9.

$$X_{s}(n) = X_{s(n-1)} + \Omega_{2} - K_{2}/2\pi \sin(2\pi X_{s(n-1)})$$

Table 2 shows the values of the computed parameters of the recognized mean maps. Further details on these three steps are described in Rezaee and Kobravi's (2020) study.

The fourth step is designing a fuzzy controller that consists of two inputs. For this purpose, we apply the Mamdani fuzzy inference system and centroid of area method for defuzzification.

The inputs of this fuzzy controller include the values of the system trajectory distance from the detected sine-circle maps related to the shank angle and the shank angular velocity, respectively. Its output regulates the excitation signal applied to the four muscles involved in walking. Figure 5 shows the block diagram of the applied control strategy.

Simulation and analysis

In this section, we examine the effects of handling existing uncertainties and imprecisions in the gait dynamics on the control quality by increasing the number of fuzzy rules, expanding the overlap of membership func-



Figure 2. The locations of the markers for tracking the shank movement by the motion analysis system

Table 2. The computed parameters of the identified mean sine-circle maps (Rezaee & Kobravi's: 2020)

Parameters	Mea	n±SD
Sine-circle map 1 (shank angle)	0.78±0.12	0.61±0.05
Sine-circle map 2 (shank angular velocity)	6.49e-008±1.40e-007	0.02±0.03
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tions, and increasing the number of fuzzy partitions. The research process is shown in Figure 6.

Increasing the number of fuzzy rules

The initial design of the fuzzy controller

In the first step, we designed a fuzzy controller with five membership functions in each input and output, without overlap, and five fuzzy rules. As seen in Figure 7, the angles obtained in the hip and knee joints are abnormal due to the crisp behavior of the controller, and the model output has distortion. In the second step, we increase the number of fuzzy rules from 5 to 25 while keeping the number of fuzzy partitions and rate of overlapping unchanged. During this phase, the angles obtained in the hip and knee joints remain within the normal range (Figure 8).

Expanding the overlap of membership functions

In the third step, we expand the overlap. The angles obtained in the hip and knee joints are in the normal range (Figure 9).



Figure 4. A Poincaré section in the phase space



Figure 3. Phase space related to one gait cycle data

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Figure 5. Block diagram related to the control strategy



Figure 6. The overview of the analysis done in this research

Abbreviations: IFC: Initial fuzzy controller; FCMR: Fuzzy controller with more rules; FCO: Fuzzy controller with overlap; FCMP: Fuzzy controller with more partitions.

Increasing the number of fuzzy partitions

In the fourth step, while the number of fuzzy rules remains constant at 25, we increase the number of fuzzy membership functions. The obtained angles in the hip and knee joints fall within the normal range (Figure 10).

The fuzzy rules database is provided in Table 3, and Figure 11 depicts the membership functions of input/output variables related to the mentioned fuzzy controllers. Also, Figure 12 shows the control surface of the mentioned fuzzy controllers.

3. Results

In this study, we evaluated the performance of the designed fuzzy controllers using a series of quantitative criteria. These criteria include the maximum amplitude of noise and step disturbances that the controller can handle while remaining stable. Additionally, we employed four quantitative criteria in the study by Rezaee and Kobravi (2020) for comparing and evaluating our controller performance, including the correlation dimension and Lyapunov exponent for the shank and thigh angles (D_c _shank, D_c_thigh, λ _shank, λ _thigh), as detailed in Table 4. We introduced explicit disturbances, such as noise and step disturbances, directly into the model to assess the robustness of our fuzzy controller. This approach differs from the study conducted by Rezaee and Kobravi (2020), where the uncertainty is implied but not explicitly addressed, and no specific disturbance tests are performed. In contrast, our study focused on investigating uncertainty and assessing the performance of the fuzzy controller under uncertain conditions and disturbance tests. We simulated real-world conditions by applying disturbances with varying amplitudes and demonstrated that our simplified fuzzy controller, which uses only two inputs, manages these challenges.

The results of the simulation and analysis are given in Table 5. Regarding the quantitative criteria related to the correlation dimension and Lyapunov exponent, in addition to the output value of the model, the absolute value of its difference from the normal level (Rezaee & Kobravi, 2020) was also included in the Table for a better comparison.

According to Table 5, the fuzzy controller with more partitions (FCMR) demonstrates increased accuracy and improved similarity to a healthy human gait compared to other fuzzy controllers. Also, the FCMR controller results in three of the four criteria (D_c _thigh, λ _shank, λ _thigh) falling within the normal range, aligning more closely with healthy gait dynamics. Although in the study by Rezaee and Kobravi (2020), there was an effort to approximate healthy walking dynamics, only one cri-

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Figure 7. The range of angles in the hip and knee joints in the initial fuzzy controller (IFC)

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terion ($D_{c_{-}}$ thigh) fell within the normal range. This outcome is attributed to the increased number of fuzzy rules and the absence of overlap in membership functions, as indicated by the correlation dimension and Lyapunov exponent values in the shank and thigh.

In contrast, fuzzy controller with more rules (FCO) exhibited an expanded overlap of membership functions, leading to increased noise and step disturbance tolerance compared to other fuzzy controllers. However, this outcome comes at the cost of reduced accuracy and a larger deviation from the walking dynamics of a healthy per-



Figure 8. The range of angles in hip and knee joints in FCMR



Figure 9. The range of angles in the hip and knee joints in fuzzy controller with overlap (FCO)

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son, as indicated by the correlation dimension and Lyapunov exponent values.

Lastly, FCMP suffers from incomplete coverage of the decision space due to an increased number of fuzzy partitions and insufficient rules. Consequently, it exhibits reduced noise and step disturbance tolerance compared to other fuzzy controllers. However, the increased number of fuzzy partitions results in improved accuracy compared to FCO and closer dynamic with normal gait dynamics, as indicated by the values of D_c_shank, $\lambda_$ shank, and $\lambda_$ thigh.



Figure 10. The range of angles in the hip and knee joints in fuzzy controller with more partitions (FCMP)

Table 3. THE rules FOR fuzzy controllers

Fuzzy Controllers				Linguistic	Variables				
	JE				E				
	dE	NB		NS	ZERO	PS		PB	
_	NB	-		NB	-	NS		-	
EC	NS -		-	-	-	-			
	ZERO	-		-	ZERO	-		-	
	PS	-		ZERO	-	PS		-	
	РВ	-		-	-	-	-		
					E				
Fuzzy Controllers	dE	NB		NS ZERO		PS		РВ	
	NB	NB		NB	NS	NS		ZERO	
Q	NS	NB		NS	NS	ZERO		PS	
FCMR & FCO	ZERO NS			NS	ZERO	PS		PS	
FCN	PS	5 NS		ZERO	PS	PS		РВ	
	РВ	ZERO		PS	PS	РВ		РВ	
					E				
Fuzzy Controllers	dE	NB	NM	NS	ZERO	PS	РМ	РВ	
	NB	NB	-	NB	NB	NM	-	ZERO	
	NM	-	-	-	-	-	-	-	
	NS	NB	-	NM	NS	ZERO	-	PM	
FCMP	ZERO	NB	-	NS	ZERO	PS	-	PB	
_	PS	NM -		ZERO	PS	PM -		PB	
	PM	-	-	-	-	-	-	-	
	PB	ZERO	_	PM	PB	PB	_	PB	

Abbreviations: IFC: Initial fuzzy controller; FCMR: Fuzzy controller with more rules; FCO: Fuzzy controller with overlap; FCMP: Fuzzy controller with more partitions.

Notes: "E" refers to the difference between the shank angle and the sine-circle map 1: and "dE" represents the difference between the shank angular velocity and the sine-circle map 2.



Figure 11. The input/output variables membership functions in fuzzy controllers

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Abbreviations: IFC: Initial fuzzy controller; FCMR; Fuzzy controller with more rules; FCO: Fuzzy controller with overlap; FCMP: Fuzzy controller with more partitions.

Note: "E" refers to the difference between the shank angle and the sine-circle map 1, and "dE" represents the difference between the shank angular velocity and the sine-circle map 2.

4. Discussion

Advantages and conclusions of the proposed work

The primary objective of rehabilitation is to establish a movement pattern that closely resembles the dynamics of a healthy individual. Regrettably, some studies overlook this crucial aspect and focus solely on generating movement in the paralyzed limb without considering the potential harm it can inflict on the neuromuscular system. However, creating effective and goal-oriented rehabilitation, capable of generating and controlling a natural and healthy dynamic, runs into various challenges. On the one hand, the employed simplifications and linearization for modeling purposes, and on the other hand, the uncertainties inherent in the dynamics of biological systems, stemming from their chaotic nature, impede the attainment of a comprehensive understanding and accurate modeling of biological phenomena. Consequently, the only viable approach to tackle this challenge is embracing the true uncertainties in the surrounding world. Rather than disregarding reality and resorting to unnecessary simplifications, the intricate behavior of biological systems arising from their inherent uncertainty should be duly acknowledged when designing the desired control strategy. Effective knowledge management in this uncertain and imprecise world necessitates using appropriate tools. In this research, our primary focus was to develop a fuzzy controller based on the gait basin of attraction concept, leveraging the methodology outlined in the previous study (Rezaee & Kobravi, 2020). We strived to streamline the design of the controller, aiming to create a simplified structure that incorporates only two inputs. However, our main objective is to emphasize the significant role of proper management of uncertainty and imprecision knowledge in gait dynamics.

The fuzzy rules used in this study are developed through a comprehensive process that integrates simulation experiments and expert knowledge. This approach ensures the final rules are accurately tuned to meet system re-

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Figure 12. The control surface of the fuzzy controllers

quirements and enhance controller performance. Our findings highlight the potential of fuzzy logic in managing the nonlinear dynamics of walking and enhancing gait performance, with implications for rehabilitation. The fuzzy logic-based controller offers a transparent structure and robust solution by effectively addressing uncertainties. This study underscores the importance of addressing these challenges and sheds light on the role of fuzzy logic in gait rehabilitation.

Although this study explicitly models and controls only two joints; using FES and ankle-foot orthoses is crucial in approximating healthy walking patterns. FES stimulates the knee and hip muscles, while the orthosis supports and stabilizes the ankle and foot, allowing the study to achieve gait patterns similar to those of a healthy subject. As shown in the results section, our investigation reveals that increasing the number of fuzzy rules and partitions enhances the output accuracy and gait dynamics' similarity to a healthy human. In contrast, incomplete coverage of the decision space due to an increased number of fuzzy partitions and insufficient rules reduces the controller's robustness. On the other hand, expanding the overlap of membership functions reduces the output accuracy but improves the robustness of the control strategy. This study demonstrates the effective management of uncertainties and imprecisions in system dynamics by adjusting the number of fuzzy rules, partitions, and membership function overlaps. Despite the simplicity of the designed controller structure with only two inputs, it outperforms the study of Rezaee and Kobravi (2020) due to its proper handling of the existing

Table 4. The mathematical equation of the applied quantitative criteria (Hilborn, 2000)

Quantitative Criteria	Mathematical Mode	Parameter			
Correlation dimension	$\begin{cases} D_c = \lim_{R \to 0} \frac{\log C(R)}{\log(R)} \\ C(R) = \frac{1}{N} \sum_{i=1}^{N} p_i(R) \\ p_i(R) = N_i/N - 1 \end{cases}$	N=number of trajectory points $p_i(R)$ =the relative number of points within the distance of the point			
Lyapunov exponent	$\begin{cases} \lambda = \frac{1}{n} ln \frac{d_n}{d_0} \\ d_n = x_{j+n} - x_{i+n} \end{cases}$	N=number of trajectory points x_i and x_j =two nearby trajectory points in state space			

		Fuzzy Controllers								
Quantitative Criteria		IFC	FCMR		FCO		FCMP		The Study by Rezaee & Kobravi (2020)	
Μ	ax tolerated noise amplitude	_	0.29		0.34		0.28		Not	
	tolerated step distur- bance amplitude	-	0.74		0.94		0.69		Not	
Qu	antitative Criteria	IFC	Difference	Value	Differ- ence	Value	Difference	Value	Difference	Value
(noi	DShank mal level 1.85 \pm 0.01)	_	0.17	1.68	0.19	1.66	0.18	1.67	0.22	1.63
(noi	D_{c} _Thigh mal level 1.78±0.02)	_	0.02	1.76	0.03	1.75	0.03	1.75	0.02	1.76
(Nor	λ _Shank mal level 2.10±0.12)	_	0.12	2.22	0.23	2.33	0.19	2.29	0.28	2.38
(nor	λ _Thigh mal level 2.64±0.17)	_	0.09	2.55	0.27	2.91	0.16	2.48	0.44	2.20
Features	Number of fuzzy rules	5	25		25		25		Not	
	Number of fuzzy partitions	5	5		5		7		Not	
	Overlapping mem- bership functions	×	×		\checkmark		\checkmark		Not	

Table 5. Comparing quantitative criteria values in the mentioned fuzzy controllers

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Abbreviations: IFC: Initial fuzzy controller; FCMR: Fuzzy controller with more rules; FCO: Fuzzy controller with overlap; FCMP: Fuzzy controller with more partitions.

Notes: D_Shank: D_Thigh: λ Shank: and λ Thigh represent the correlation dimension and Lyapunov exponent for the shank and thigh angles: respectively. The difference indicates the absolute value of the difference between the mentioned criteria related to the model output and their normal values in the presence of each controller. "Not" indicates that the test was not conducted in the mentioned study. The best results: which indicate that our criterion falls within the normal range of a healthy person: are shown in bold. Due to the invalid output of controller 1, the specified criteria have not been calculated, and a "-" mark has been assigned to the respective sections.

uncertainties and imprecisions in walking dynamics. In other words, these results indicate that a well-designed fuzzy controller, even with a simplified structure, can maintain stability and accuracy under challenging conditions. This improvement is due to the careful design of fuzzy rules, appropriate partitioning, and proper overlap of membership functions, which provide a more resilient control strategy.

Limitations of the proposed work

Whereas the study dataset was acquired from five volunteers during three uninterrupted gait cycles, more participants with different ages and genders and more gait cycles were needed to conclude the process accurately.

Future works

The employed control strategy can be used not only for people who are completely paralyzed but also for people who have muscle weakness. We hope to integrate the proposed strategy with an exoskeleton robot at the next step of this research. Also, we intend to consider the controller output as multi-variable in the future so that a separate control signal applies to each of the agonist and antagonist muscles of the knee and hip joints.

Ethical Considerations

Compliance with ethical guidelines

As this study used data from Rezaee and Kobravi's (2020) study, ethical approval was not required.

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Authors' contributions

Conceptualization, methodology, visualization, and visualization, All authors; Data curation, formal analysis, software, writing the original draft, Zohre Rezaee; Supervision, review and editing: Mohammad-R Akbarzadeh-T.

Conflict of interest

The authors declared no conflict of interest.

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